

## TITLE OF THE INVENTION

Heat Resistant Coated Member, Making Method, and  
Treatment Using the Same

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## BACKGROUND OF THE INVENTION

### Technical Field

This invention relates to a heat resistant coated  
10 member which is used in the sintering or heat treatment of  
powder metallurgical metal, cermet or ceramic materials in  
vacuum or an inert or reducing atmosphere; a method for  
preparing the same; and a method for the heat treatment of  
powder metallurgical metal, cermet or ceramic materials using  
15 the coated member.

### Background Art

Powder metallurgy products are generally manufactured  
by mixing a primary alloy with a binder phase-forming powder,  
20 then kneading the mixture, followed by compaction, sintering  
and post-treatment. The sintering step is carried out in a  
vacuum or an inert gas atmosphere, and at an elevated  
temperature of 1,000 to 1,600°C.

In a typical cemented carbide manufacturing process,  
25 solid solutions of tungsten carbide with cobalt, titanium  
carbide, and tantalum carbide are comminuted and mixed, then  
subjected to drying and granulation to produce a granulated  
powder. The powder is then pressed, following which such  
steps as dewaxing, pre-sintering, sintering and machining are  
30 carried out to give the final cemented carbide product.

Sintering is carried out at or above the temperature  
at which the cemented carbide liquid phase appears. For  
example, the eutectic temperature for a ternary WC-Co system  
is 1,298°C. The sintering temperature is generally within a  
35 range of 1,350 to 1,550°C. In the sintering step, it is  
important to control the atmosphere so that cemented carbide

correctly containing the target amount of carbon may be stably sintered.

When cemented carbide is produced by sintering at about 1,500°C, green specimens placed on a carbon tray often react with the tray. That is, a process known as carburizing occurs, in which carbon from the tray impregnates the specimen, lowering the strength of the specimen. A number of attempts have been made to avoid this type of problem, either by choosing another type of tray material or by providing on the surface of the tray a barrier layer composed of a material that does not react with the green specimen. For example, ceramic powders such as zirconia, alumina and yttria are commonly used when sintering cemented carbide materials. One way of forming a barrier is to scatter the ceramic powder over the tray and use it as a placing powder. Another way is to mix the ceramic powder with a solvent and spray-coat the mixture onto the tray or apply it thereto as a highly viscous slurry. Yet another way is to form a coat by using a thermal spraying or other suitable process to deposit a dense ceramic film onto the tray. Providing such an oxide layer as a barrier layer on the surface of the tray has sometimes helped to prevent reaction of the tray with the specimen.

In general, the powder metallurgy or ceramic manufacturing process involves firing or sintering and heat treatment steps. The specimen that is to become a product is set on the tray. Since the specimen can react with the tray material to invite a deformation or compositional shift or introduce impurities into the product, there are many cases where products are not fired or sintered in high yields. There are many ways for preventing the reaction of the tray with the product, as described above. For example, an oxide powder such as alumina or yttria or a nitride powder such as aluminum nitride or boron nitride is used as the placing powder. Alternatively, such an oxide or nitride powder is mixed with an organic solvent to form a slurry, which is coated or sprayed to the tray to form a coating on the tray for preventing the tray from reacting with the product. On

use of placing powder, however, some of the placing powder will deposit on the product. The slurry coating procedure must be repeated every one or several sintering steps because the coating peels from the substrate (tray).

5           To solve these problems, JP-A 2000-509102 proposes to form a dense coating on the surface of a tray by a thermal spraying technique. Specifically, when a graphite tray is used in the sintering of materials to produce cemented carbides or cermets, the graphite tray is coated with a cover  
10 layer made of  $Y_2O_3$  containing up to 20% by weight of  $ZrO_2$  or an equivalent volume of another heat resistant oxide such as  $Al_2O_3$  or a combination thereof, and having an average thickness of at least 10  $\mu m$ .

          Although the thermally sprayed coating of this patent  
15 publication is effective for preventing reaction with the product, there is a likelihood that the coating readily peels off due to thermal degradation at the interface between the coating and the tray substrate by repeated thermal cycling. It is thus desired to have a coated member in which the oxide  
20 coating does not peel from the substrate even when subjected to repeated thermal cycling, that is, having heat resistance, corrosion resistance, durability and non-reactivity.

          More particularly, even when a barrier layer is formed on a carbon tray, reaction can occur between the barrier  
25 layer and the tray. After one or a few sintering cycles, the barrier layer cracks, fragments and spalls off. Peeling of the coating allows for reaction between the carbon tray and a specimen. During the sintering step, the coating can peel and fragment into pieces which are often introduced into the  
30 specimen. Then a fresh coated tray must be used.

          For the above-described reason, there is a need for a tray having a long lifetime in that when used in sintering, the barrier layer does not react with a specimen or with the tray substrate or peel off, and when used in the sintering of  
35 powder metallurgical products, the barrier layer does not react with specimens or peel from the tray substrate even after repeated use.

## SUMMARY OF THE INVENTION

An object of the present invention is to provide a coated member which exhibits excellent heat resistance, corrosion resistance, and non-reactivity when used in the sintering or heat treatment of powder metallurgical metal, cermet or ceramic materials in vacuum or an inert or reducing atmosphere. Another object is to provide a method for preparing the coated member. A further object is to provide a method of heat treatment using the coated member.

It has been found that a heat resistant coated member in which a substrate of a material selected from among Mo, Ta, W, Zr, and carbon is coated with a rare earth-containing oxide exhibits excellent heat resistance, corrosion resistance, and non-reactivity when used in the sintering or heat treatment of a powder metallurgical metal, cermet or ceramic material in vacuum or an inert or reducing atmosphere. When a surface layer of the rare earth-containing oxide coating has a hardness of at least 50 HV in Vickers hardness, the separation of the oxide coating from the substrate is prohibited. When the surface layer has a surface roughness of up to 20  $\mu\text{m}$  in centerline average roughness Ra, the coated member is more effective for preventing a ceramic product from deformation during sintering or heat treatment thereon.

It has also been found that a heat resistant coated member in which a substrate having a coefficient of linear expansion of at least  $4 \times 10^{-6}$  (1/K) is coated with a rare earth-containing oxide exhibits heat resistance, durability (the coating scarcely peels off upon repeated thermal cycling) and non-reactivity to a product, when used in the sintering or heat treatment of a powder metallurgical metal, cermet or ceramic material in vacuum or an inert or reducing atmosphere.

It has further been found that a heat resistant coated member in which a heat resistant substrate is coated with a layer of a specific composition comprising a complex oxide of a lanthanoid element and a Group 3B element such as Al, B or Ga exhibits heat resistance, durability (the coating scarcely

peels off upon repeated thermal cycling), non-reactivity to a product and anti-sticking, when used in the sintering or heat treatment of a powder metallurgical metal, cermet or ceramic material in vacuum or an inert or reducing atmosphere.

5 In a first embodiment, the present invention provides

(1) a heat resistant coated member comprising a substrate made of a material selected from the group consisting of Mo, Ta, W, Zr, and carbon and a coating of rare earth-containing oxide thereon, the rare earth-containing  
10 oxide coating including a surface layer having a hardness of at least 50 HV in Vickers hardness.

Also provided are (2) a method for preparing a heat resistant coated member comprising coating a substrate made of a material selected from the group consisting of Mo, Ta, W,  
15 Zr, and carbon with a rare earth-containing oxide, and heat treating the surface of the coating so that the surface has a hardness of at least 50 HV in Vickers hardness; and

(3) a method of heat treating a powder metallurgical metal, cermet or ceramic material, comprising the steps of  
20 placing the material on the heat resistant coated member of claim 1 and heat treating the material thereon.

In a second embodiment, the present invention provides

(4) a heat resistant coated member comprising a substrate having a coefficient of linear expansion of at  
25 least  $4 \times 10^{-6}$  (1/K) and a layer comprising, preferably consisting of, rare earth-containing oxide coated thereon.

Preferably the coating layer comprises at least 80% by weight of a rare earth oxide and the balance of another metal oxide which is mixed, combined or laminated therewith. Also  
30 preferably, the rare earth oxide is mainly composed of an oxide of at least one element selected from the group consisting of Dy, Ho, Er, Tm, Yb, Lu, and Gd.

In a typical application, the coated member is used in the sintering of a powder metallurgical metal, cermet or  
35 ceramic material in vacuum or an inert or reducing atmosphere.

In a third embodiment, the present invention provides the coated members defined below.

(5) A heat resistant coated member comprising a metal, carbon, or carbide, nitride or oxide ceramic substrate; an intermediate coating layer on the substrate comprising a lanthanoid oxide, an oxide of Y, Zr, Al or Si, a mixture of these oxides, or a complex oxide of these elements; and a coating layer on the intermediate coating layer comprising a complex oxide of a lanthanoid element and a Group 3B element.

(6) A heat resistant coated member comprising a metal, carbon, or carbide, nitride or oxide ceramic substrate; an intermediate coating layer on the substrate comprising a lanthanoid oxide, an oxide of Y, Zr, Al or Si, a mixture of these oxides, or a complex oxide of these elements; and a coating layer on the intermediate coating layer comprising a complex oxide of yttrium, an optional lanthanoid element and a Group 3B element.

(7) A heat resistant coated member comprising a metal, carbon, or carbide, nitride or oxide ceramic substrate; an intermediate coating layer on the substrate comprising a metal selected from the group consisting of Mo, W, Nb, Zr, Ta, Si and B, or a carbide or nitride thereof; and a coating layer on the intermediate coating layer comprising a complex oxide of a lanthanoid element and a Group 3B element.

(8) A heat resistant coated member comprising a metal, carbon, or carbide, nitride or oxide ceramic substrate; an intermediate coating layer on the substrate comprising a metal selected from the group consisting of Mo, W, Nb, Zr, Ta, Si and B, or a carbide or nitride thereof; and a coating layer on the intermediate coating layer comprising a complex oxide of yttrium, an optional lanthanoid element and a Group 3B element.

(9) A heat resistant coated member comprising a metal, carbon, or carbide, nitride or oxide ceramic substrate; an intermediate coating layer on the substrate comprising  $ZrO_2$ ,  $Y_2O_3$ ,  $Al_2O_3$  or a lanthanoid oxide, a mixture of these oxides, or a complex oxide of Zr, Y, Al or lanthanoid element, and a

metal selected from the group consisting of Mo, W, Nb, Zr, Ta, Si and B; and a coating layer on the intermediate coating layer comprising a complex oxide of a lanthanoid element and a Group 3B element.

5           (10) A heat resistant coated member comprising a metal, carbon, or carbide, nitride or oxide ceramic substrate; an intermediate coating layer on the substrate comprising  $ZrO_2$ ,  $Y_2O_3$ ,  $Al_2O_3$  or a lanthanoid oxide, a mixture of these oxides, or a complex oxide of Zr, Y, Al or  
10 lanthanoid element, and a metal selected from the group consisting of Mo, W, Nb, Zr, Ta, Si and B; and a coating layer on the intermediate coating layer comprising a complex oxide of yttrium, an optional lanthanoid element and a Group 3B element.

15           Preferably, the complex oxide of yttrium and a Group 3B element contains up to 80% by weight of  $Y_2O_3$  and at least 20% by weight of  $Al_2O_3$ .

          (11) A heat resistant coated member comprising a metal, carbon, or carbide, nitride or oxide ceramic  
20 substrate; an intermediate coating layer on the substrate comprising a lanthanoid oxide, an oxide of Y, Zr, Al or Si, a mixture of these oxides, or a complex oxide of these elements; and a coating layer on the intermediate coating layer comprising an oxide of a lanthanoid element, aluminum  
25 or yttrium.

          (12) A heat resistant coated member comprising a metal, carbon, or carbide, nitride or oxide ceramic substrate; an intermediate coating layer on the substrate comprising a metal selected from the group consisting of Mo,  
30 W, Nb, Zr, Ta, Si and B, or a carbide or nitride thereof; and a coating layer on the intermediate coating layer comprising aluminum oxide or a lanthanoid oxide.

More specific embodiments as described below are also provided.

35           (13) A heat resistant coated member comprising a carbon substrate, an interlayer of  $Yb_2O_3$  formed thereon, and a coating layer formed on the interlayer and comprising a

complex oxide consisting essentially of up to 80% by weight of  $Y_2O_3$  and at least 20% by weight of  $Al_2O_3$ .

(14) A heat resistant coated member comprising a carbon substrate, an interlayer of  $ZrO_2$  formed thereon, and a coating layer formed on the interlayer and comprising a complex oxide consisting essentially of up to 80% by weight of  $Y_2O_3$  and at least 20% by weight of  $Al_2O_3$ .

(15) A heat resistant coated member comprising a carbon substrate, an interlayer of  $ZrO_2$  and  $Y_2O_3$  formed thereon, and a coating layer formed on the interlayer and comprising a complex oxide consisting essentially of up to 80% by weight of  $Y_2O_3$  and at least 20% by weight of  $Al_2O_3$ .

(16) A heat resistant coated member comprising a carbon substrate, an interlayer of tungsten formed thereon, and a coating layer formed on the interlayer and comprising a complex oxide consisting essentially of up to 80% by weight of  $Y_2O_3$  and at least 20% by weight of  $Al_2O_3$ .

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

In the first embodiment of the invention, the heat resistant coated member includes a substrate made of a material selected from among molybdenum Mo, tantalum Ta, tungsten W, zirconium Zr, and carbon C and a layer of rare earth-containing oxide coated thereon. The coated member is intended for use in the sintering or heat treatment of powder metallurgical metals, cermets or ceramics in vacuum or an inert or reducing atmosphere to form a cemented carbide or similar product. It is recommended that the type of substrate, the type of coating oxide, and the combination thereof be varied and optimized in accordance with the product itself and the temperature and gas used in sintering and heat treatment.

The coated member of the invention is particularly effective as crucibles for melting metal or as jigs for fabricating and sintering various types of complex oxides. Examples of such jigs include setters, saggars, trays and molds.



In the invention, the substrate for forming such heat-resistant, corrosion-resistant members used in the sintering or heat treatment of powder metallurgical metals, cermets and ceramics is made of a material selected from  
5 among molybdenum, tantalum, tungsten, zirconium, and carbon.

When carbon is used as the substrate, the carbon substrate has a density of preferably at least  $1.5 \text{ g/cm}^3$ , more preferably at least  $1.6 \text{ g/cm}^3$ , and most preferably at least  $1.7 \text{ g/cm}^3$ . Note that carbon has a true density of  $2.26 \text{ g/cm}^3$ .  
10  $\text{g/cm}^3$ . At a substrate density of less than  $1.5 \text{ g/cm}^3$ , although the low density provides the substrate with good resistance to thermal shock, the porosity is high, which makes the substrate more likely to adsorb air-borne moisture and carbon dioxide and sometimes results in the release of  
15 adsorbed moisture and carbon dioxide in a vacuum.

When a transparent ceramic such as YAG is sintered, treatment within a temperature range of  $1,500$  to  $1,800^\circ\text{C}$  in a vacuum, an inert atmosphere or a weakly reducing atmosphere tends to give rise to reactions between the substrate  
20 material and the coating oxide and to reactions between the coating oxide and the product on account of the elevated temperature. It is therefore important to select a substrate and coating oxide combination that discourages such reactions from arising. At temperatures above  $1,500^\circ\text{C}$  in particular,  
25 when carbon is used in the substrate, aluminum and rare-earth elements tend to form carbides in a vacuum or a reducing atmosphere. Under such conditions, it is desirable to use a coated jig in which a molybdenum, tantalum or tungsten substrate is combined with a rare-earth-containing oxide as  
30 the oxide coating.

In this regard, the substrate preferably has a coefficient of linear expansion of at least  $4 \times 10^{-6} (1/\text{K})$ . Then the heat resistant coated member in the second embodiment of the invention is defined as comprising a  
35 substrate having a coefficient of linear expansion in the range and a layer of rare earth-containing oxide coated thereon.

More specifically, in the second embodiment, a substrate having a coefficient of linear expansion of at least  $4 \times 10^{-6}$  (1/K) is used as the substrate for forming a coated member having heat resistance, corrosion resistance and durability for use in the sintering or heat treatment of powder metallurgical metals, cermets or ceramics. The preferred substrate has a coefficient of linear expansion of  $4 \times 10^{-6}$  to  $50 \times 10^{-6}$  (1/K), more preferably  $4 \times 10^{-6}$  to  $20 \times 10^{-6}$  (1/K). As used herein, the coefficient of linear expansion is a coefficient of thermal expansion of a solid as is well known in the art. It is given by the equation:

$$\alpha = (1/L_0) \times (dL/dt) \text{ wherein } L_0 \text{ is a length at } 0^\circ\text{C, and } L \text{ is a length at } t^\circ\text{C.}$$

It is noted that the coefficient of linear expansion used herein is an average measurement over a temperature range of 20 to  $100^\circ\text{C}$ .

Rare earth-containing oxides which are effective as the protective coating for preventing reaction with powder metallurgical products, cermet products or ceramic products generally have a coefficient of linear expansion of  $4 \times 10^{-6}$  to  $8 \times 10^{-6}$  (1/K) in a temperature range of 20 to  $400^\circ\text{C}$ . When a coating is formed on a substrate from such a rare earth-containing oxide by a thermal spraying technique, it is important that the coefficient of linear expansion of the substrate be equal to or greater than that of the rare earth-containing oxide coating. Such adjustment restrains the coating from delamination by thermal cycling. This is due to the anchoring effect known in the thermal spraying art.

Selection of a substrate having a higher coefficient of linear expansion than a coating enhances the anchoring effect. It should be understood that the type of substrate material which can be used is limited in certain cases because the melting point and atmosphere resistance of the substrate must also be taken into account depending on the firing or sintering temperature and atmosphere or the heat treating temperature and atmosphere to which powder

metallurgical products, cermet products or ceramic products are subjected.

For example, a carbon substrate is a typical substrate to be used in a vacuum atmosphere at 1400 to 1600°C. The carbon substrate is widely used for sintering because it has a low density or a light weight, and a high strength and is easily machinable. When carbon is used as a substrate to be covered with an oxide coating, the substrate should preferably have a coefficient of linear expansion of at least  $4 \times 10^{-6}$  (1/K). If the coefficient of linear expansion is less than  $4 \times 10^{-6}$  (1/K), the anchoring effect becomes weak, with a likelihood for the thermally sprayed coating to peel upon thermal cycling to a high temperature of at least 1400°C.

The coefficient of linear expansion of a carbon substrate is closely related to the density of the carbon substrate and the particle size and crystallinity of primary particles of which the carbon substrate is made. Even when the substrate has a high density, the coefficient of linear expansion varies with the particle size and crystallinity of primary particles of which the substrate is made. Thus, a mere choice of a high density carbon substrate is insufficient because the anchoring effect is weak if the coefficient of linear expansion is less than  $4 \times 10^{-6}$  (1/K), with a likelihood for the thermally sprayed coating to peel upon thermal cycling to a high temperature of at least 1400°C.

When a transparent ceramic such as YAG is sintered, treatment within a temperature range of 1,500 to 1,800°C in a vacuum, an inert atmosphere or a weakly reducing atmosphere tends to give rise to reactions between the substrate material and the coating oxide and to reactions between the coating oxide and the product on account of the elevated temperature. It is therefore important to select a substrate and coating oxide combination that discourages such reactions from arising. At temperatures above 1,500°C in particular, when carbon is used in the substrate, aluminum and rare-earth

elements tend to form carbides in a vacuum or a reducing atmosphere. Under such conditions, it is desirable to use a coated jig in which a molybdenum, tantalum or tungsten substrate is combined with a rare-earth-containing oxide as  
5 the oxide coating.

In the first and second embodiments, the substrate has a density of preferably at least 1.5 g/cm<sup>3</sup>, and especially 1.7 to 20 g/cm<sup>3</sup>.

The coated members of the first and second embodiments  
10 have a layer of rare earth-containing oxide coated on the substrate. The rare earth-containing oxide used herein is an oxide containing a rare earth element or elements; that is, an element selected from among those having the atomic numbers 57 to 71.

15 In the coated member of the first embodiment, the substrate is preferably coated with an oxide of at least one rare earth element selected from among Sm, Eu, Gd, Dy, Ho, Er, Tm, Yb, and Lu, more preferably an oxide of Er, Tm, Yb or Lu.

20 In the coated member of the second embodiment, the substrate is preferably coated with an oxide of at least one rare earth element selected from among Dy, Ho, Er, Tm, Yb, Lu and Gd, more preferably an oxide of Er, Tm, Yb, Lu or Gd. This is because oxides of light to medium rare earth elements  
25 ranging from La to Tb undergo transitions in their crystalline structures below 1,500°C, by which transition the coating becomes brittle and liable to peel off to contaminate the product or the apparatus, or some oxides are reactive with carbon.

30 The oxide coating may consist of one or more rare earth oxides. Alternatively, in the oxide coating, an oxide of a metal selected from Group 3A to Group 8 elements may be mixed, combined or laminated with the rare earth oxide in an amount of up to 20% by weight, and especially up to 18% by  
35 weight. More preferably, an oxide of at least one metal selected from among Al, Si, Zr, Fe, Ti, Mn, V, and Y is used.

The rare earth-containing oxide used herein is preferably in the form of particles having an average particle size of 10 to 70  $\mu\text{m}$ . The coated member is preferably prepared by plasma spraying or flame spraying a rare earth-containing material in an inert atmosphere such as argon to deposit a coating of rare earth-containing oxide on the substrate. If necessary, the substrate is surface treated by a suitable technique such as blasting prior to the thermal spraying.

Alternatively, the coated member is prepared by pressing rare earth-containing oxide particles having an average particle size of 10 to 70  $\mu\text{m}$  in a mold to form a preform, heat treating the preform and attaching it to the substrate.

The coating of rare earth-containing oxide has a thickness of 0.02 mm to 0.4 mm, more preferably 0.1 mm to 0.2 mm when it is thermally sprayed. At less than 0.02 mm, there is a possibility that on repeated use of the coated member, the substrate may react with the material being sintered. On the other hand, at more than 0.4 mm, thermal shock within the coated oxide film may cause the oxide to delaminate, possibly resulting in contamination of the product. In case the coated member has the heat treated preform attached to the substrate, the thickness of the oxide layer is not particularly limited though a thickness of 0.3 to 10 mm, especially 1 to 5 mm is preferred.

In the first embodiment, the surface of the oxide coating is preferably heat treated in an oxidizing atmosphere, vacuum or inert gas atmosphere at a high temperature of 1,200 to 2,500°C, more preferably 1,200 to 2,000°C. For example, the surface of the thermally sprayed coating is roasted by an argon/hydrogen plasma flame and at a temperature near its melting point. By this heat treatment, the surface of the coating is partially melted and thus smoothed to a surface roughness of 10  $\mu\text{m}$  or less. With heat treatment below 1,200°C or without heat treatment, the

coating surface may not be smoothed to a desired level of surface roughness. Heat treatment above 2,500°C or above the melting point of the sprayed coating is undesirable because the oxide coating can be melted or evaporated.

5           Through the heat treatment, the rare earth-containing oxide coating layer in the form of a preform or thermally sprayed coating is increased in hardness, thereby preventing a product being fired from fusing thereto or preventing the coating from peeling off.

10           In the coated member of the first embodiment, the rare earth-containing oxide coating includes a surface layer having a hardness of at least 50 in Vickers hardness (HV). Preferably the surface layer has a Vickers hardness of at least 80, more preferably at least 100, even more preferably  
15           at least 150. The upper limit of Vickers hardness is not critical, but is generally up to 3000, preferably up to 2500, more preferably up to 2000, even more preferably up to 1500. With too low a surface hardness, when a material on the coated member is fired, the material being fired fuses to the  
20           rare earth-containing oxide coating so that a surface portion of the rare earth-containing oxide coating can eventually be stripped or torn off. With too high a surface hardness, the rare earth-containing oxide coating layer may crack.

          Preferably, the surface layer of the oxide coating has  
25           a surface roughness of up to 20  $\mu\text{m}$  in centerline average roughness Ra. In the case of a thermally sprayed coating, a surface roughness (Ra) in the range of 2 to 20  $\mu\text{m}$ , especially in the range of 3 to 10  $\mu\text{m}$  is preferred for effective sintering of a material thereon. At a surface roughness of  
30           less than 2  $\mu\text{m}$ , the coating layer is so flat that this may interfere with sintering shrinkage by the material resting thereon. A surface roughness of more than 20  $\mu\text{m}$  may allow the material to deform during the sintering.

          When the preform of rare earth-containing oxide  
35           particles is heat treated and attached to the substrate to construct the coated member, the heat treated preform has a

very high hardness which permits a powder metallurgical metal, cermet or ceramic material to be effectively sintered on the coated member independent of its surface roughness.

It is also possible that an oxide be thermally sprayed to form an oxide coating having a surface roughness (Ra) of at least 2  $\mu\text{m}$ , which is optionally surface worked as by polishing.

In the third embodiment, the heat resistant coated member includes a substrate which is coated with a specific layer, typically a layer of a complex oxide of yttrium or a lanthanoid element and a Group 3B element.

The substrate for forming the heat-resistant, corrosion-resistant, durable member for use in the sintering or heat treatment of powder metallurgical metals, cermets or ceramics is selected from among refractory metals (e.g., molybdenum, tantalum, tungsten, zirconium, and titanium), carbon, alloys thereof, oxide ceramics (e.g., alumina and mullite), carbide ceramics (e.g., silicon carbide and boron carbide) and nitride ceramics (e.g., silicon nitride).

In the third embodiment, an intermediate coating layer is formed on the substrate. The intermediate coating layers which can be used herein include:

- (i) a layer of a lanthanoid oxide, an oxide of Y, Zr, Al or Si, a mixture of these oxides, or a complex oxide of these elements,
- (ii) a layer of a metal selected from among Mo, W, Nb, Zr, Ta, Si and B, or a carbide or nitride thereof, and
- (iii) a layer of  $\text{ZrO}_2$ ,  $\text{Y}_2\text{O}_3$ ,  $\text{Al}_2\text{O}_3$ , or a lanthanoid oxide, a mixture of these oxides, or a complex oxide of Zr, Y, Al or lanthanoid element, and a metal element selected from among Mo, W, Nb, Zr, Ta, Si and B.

In the intermediate coating layer (iii), the proportion of oxide and metal element, as expressed by  $[(\text{oxides})/(\text{oxides} + \text{metal elements})]$ , is preferably from 30 to 70% by weight.

According to the invention, a topcoat layer is formed on the intermediate coating layer. If a topcoat layer is

formed directly on a substrate without forming an intermediate coating layer, there is a case that when a cemented carbide-forming material is rested on the topcoat layer and sintered at 1,300 to 1,500°C in vacuum or in an inert atmosphere or weakly reducing atmosphere, a likelihood of reaction between the substrate material and the topcoat layer arises depending on the sintering temperature and atmosphere. Particularly when carbon is used as the substrate material, reaction is likely to occur at temperatures above 1,400°C. Through reaction with carbon, aluminum oxide undergoes vigorous decomposition and evaporation and separates from the substrate. Some lanthanoid elements are likely to form carbides in vacuum. Once converted to a carbide, the oxide coating may readily peel from the substrate.

Then, for the purpose of inhibiting decomposition and evaporation or restraining carbide formation, an intermediate coating layer is formed on the carbon substrate as the interlayer using a refractory metal such as Mo, Ta, W or Si, a lanthanoid oxide which will not readily form a carbide with carbon, such as Eu or Yb oxide, or a mixture of a refractory metal and a lanthanoid oxide or another oxide such as  $ZrO_2$  or  $Al_2O_3$  as listed above in (i) to (iii). A topcoat layer (iv) to (vii) to be described later, for example, a coating layer of a complex oxide of Al and Y or a complex oxide of Al and lanthanoid, or a coating of lanthanoid oxide, aluminum oxide, zirconium oxide or yttrium oxide, or a coating of a compound or mixture thereof is formed on the intermediate coating layer for preventing separation at the carbon interface or preventing a cemented carbide product from sticking to the coated member.

The main component of the interlayer is desirably tungsten W for the metal layer or  $Yb_2O_3$  and/or  $ZrO_2$  for the oxide layer.

The provision of the intermediate coating layer (i) to (iii) of metal, oxide, carbide, nitride or the like enhances the interfacial bonding force to the substrate against



repeated thermal cycling. When a refractory metal such as W or Si is used as the interlayer, the refractory metal reacts with the carbon substrate to form a carbide during heat treatment at 1,450°C or higher. Specifically, tungsten  
5 converts to tungsten carbide WC, and silicon converts to silicon carbide SiC. In the case of Si, it converts to silicon nitride if treated in a nitrogen atmosphere. The conversion of the interface between the carbon substrate and the refractory metal to carbide or nitride significantly  
10 improves the bonding force to the substrate.

Further, the provision of the intermediate coating layer is effective for restraining decomposition and evaporation or carbide formation of  $Y_2O_3$ , lanthanoid oxides (e.g.,  $Gd_2O_3$ ) and  $Al_2O_3$  which are likely to react with carbon  
15 in vacuum.

For the above reasons and other, it becomes possible to prevent sticking of the coated member to a product to be fired, evaporation of the topcoat layer, and separation of the topcoat layer from the substrate. Thus a coated jig  
20 having an oxide or complex oxide coating formed on the intermediate coating layer is available.

The lanthanoid oxide for use in the formation of the intermediate coating layer is an oxide of a rare earth element selected from among those having the atomic numbers  
25 57 to 71. In addition to the rare earth oxide, an oxide of a metal selected from Groups 3A to 8 may be mixed or combined or laminated. Further preferably, an oxide of at least one metal selected from among Al, Si, Zr, Fe, Ti, Mn, V, and Y may be used.

30 In the invention, the topcoat layer is formed on the intermediate coating layer. The topcoat layers which can be used herein include:

- (iv) a layer containing a complex oxide of a lanthanoid element and a Group 3B element,
- 35 (v) a layer containing a complex oxide of yttrium and a Group 3B element,

(vi) a layer containing a complex oxide of yttrium, a lanthanoid element and a Group 3B element, and  
(vii) a layer containing an oxide of a lanthanoid element, aluminum or yttrium.

5           The layer (iv) may further contain a lanthanoid oxide and/or a Group 3B element oxide; the layer (v) may further contain yttrium oxide and/or a Group 3B element oxide; and the layer (vi) may further contain yttrium oxide, a lanthanoid oxide or a Group 3B element oxide or a mixture of  
10 these oxides.

          The lanthanoid elements are rare earth elements having the atomic numbers 57 to 71. The Group 3B elements designate B, Al, Ga, In and Tl. Formation of a complex oxide of these elements prevents the coated member from reacting with or  
15 sticking to a product being sintered. This is true particularly when a tungsten carbide material, a typical cemented carbide-forming material is fired, because reaction with tungsten or cobalt in the tungsten carbide is prevented and sticking is prevented. The risk of separation of the  
20 coating layer from the substrate as a result of sticking of the product is eliminated, and a coated member for firing having durability to thermal cycling is obtainable.

          Among the Group 3B elements, a complex oxide of aluminum and yttrium is desirable. A complex oxide of  
25 aluminum and a lanthanoid element selected from among Sm, Eu, Gd, Dy, Er, Yb and Lu is especially desirable.

          In the coating layers (iv) to (vi), the proportion of yttrium and/or lanthanoid element and Group 3B element, as expressed by  $(\text{yttrium and/or lanthanoid element})/(\text{yttrium and/or lanthanoid element} + \text{Group 3B element})$ , is preferably  
30 10 to 90% by weight. With too much Group 3B element, the bonding force of the coating layer to the substrate may be reduced by heat treatment, allowing the coating layer to separate. Too low a proportion of Group 3B element may allow  
35 the coating to seize the cemented carbide-forming material.

          With respect to the weight proportion of the complex oxide of yttrium and aluminum, the complex oxide preferably

consists of up to 80 wt% of  $Y_2O_3$  component and at least 20 wt% of  $Al_2O_3$  component. More preferably, the complex oxide consists of 70 to 30 wt% of  $Y_2O_3$  component and 30 to 70 wt% of  $Al_2O_3$  component. With more than 80 wt% of  $Y_2O_3$  component, the coating is likely to seize the cemented carbide-forming material due to a reduced content of  $Al_2O_3$  component. Too much  $Al_2O_3$  component, the bonding force of the coating layer to the substrate may be extremely reduced by heat treatment, allowing the coating layer to separate.

The intermediate coating layer and topcoat layer are formed preferably by thermal spraying. That is, these coating layers can be formed as thermally sprayed films. The thermal spraying may be routinely carried out by well-known techniques. Source particles such as complex oxide, oxide or metal particles used to form the thermally sprayed films may have an average particle size of 10 to 70  $\mu m$ . Source particles are plasma or flame sprayed onto the above-described substrate in an inert atmosphere of argon or nitrogen, thereby forming a coated member within the scope of the invention. If necessary, the surface of the substrate may be treated by a suitable technique such as blasting prior to the thermal spraying operation. It is also possible to subject the substrate surface to blasting, form an intermediate coating layer of a refractory metal, carbide or nitride on the substrate, subject the intermediate coating layer to blasting again, and form a topcoat layer of oxide or complex oxide thereon. Understandably, equivalent results are obtained by a coating technique other than thermal spraying, such as slurry coating.

The total thickness of the intermediate coating layer and topcoat layer is preferably from 0.02 mm to 0.4 mm, more preferably from 0.1 mm to 0.2 mm. A total thickness of less than 0.02 mm may leave a possibility of reaction between the substrate and the material to be sintered after repeated use. At a total thickness of more than 0.4 mm, thermal shock within the coated oxide film may cause the oxide to delaminate, possibly resulting in contamination of the

product. The thickness of the intermediate coating layer is preferably  $1/2$  to  $1/10$ , more preferably  $1/3$  to  $1/5$  of the total thickness because the intermediate coating layer in such a range exerts its effect to a full extent.

5       The heat resistant coated member produced in the foregoing manner according to the first to third embodiments of the invention may be used to effectively heat-treat or sinter powder metallurgical metals, cermets and ceramics at a temperature of up to  $2,000^{\circ}\text{C}$ , and preferably  $1,000$  to  
10  $1,800^{\circ}\text{C}$ , for 1 to 50 hours. The heat treatment or sintering atmosphere is preferably a vacuum or an inert or reducing atmosphere.

Typically the coated member of the invention is used in the heat treatment (especially firing or sintering) of  
15 metals or ceramics as mentioned above. More specifically, a metal or ceramic material to be heat treated is placed on the coated member, whereupon the material is heated or sintered at a temperature in the above-described range, and in the case of the first or second embodiment, at a temperature of  
20 up to  $1,800^{\circ}\text{C}$ , especially  $900$  to  $1,700^{\circ}\text{C}$ , for 1 to 50 hours. The heat treating or sintering atmosphere is preferably a vacuum or an inert atmosphere having an oxygen partial pressure of not more than  $0.01\text{ MPa}$  or a reducing atmosphere.

Exemplary metals and ceramics include chromium alloys,  
25 molybdenum alloys, tungsten carbide, silicon carbide, silicon nitride, titanium boride, silicon oxide, rare earth-aluminum complex oxides, rare earth-transition metal alloys, titanium alloys, rare earth oxides, and rare earth complex oxides. The coated members of the invention, typically in the form of  
30 jigs, are effective especially in the production of tungsten carbide, rare earth oxides, rare earth-aluminum complex oxides, and rare earth-transition metal alloys. More specifically, the coated members of the invention are effective in the production of magnetically permeable  
35 ceramics such as YAG and cemented carbides such as tungsten carbide, the production of Sm-Co alloys, Nd-Fe-B alloys and Sm-Fe-N alloys used in sintered magnets, and the production

of Tb-Dy-Fe alloys used in sintered magnetostrictive materials and Er-Ni alloys used in sintered regenerators.

Examples of suitable inert atmospheres include argon and nitrogen (N<sub>2</sub>) atmospheres. Examples of suitable reducing atmospheres include hydrogen gas, inert gas atmospheres in which a carbon heater is used, and inert gas atmospheres containing also several percent of hydrogen gas. An oxygen partial pressure of not more than 0.01 MPa ensures that the coated members are kept resistant to corrosion during the heat treating or sintering operation.

In addition to having a good heat resistance, the coated member of the invention also has a good corrosion resistance and non-reactivity, and can therefore be effectively used for sintering or heat-treating powder metallurgical metals, cermets or ceramics in a vacuum, an inert atmosphere or a reducing atmosphere. Where the surface layer of the rare earth-containing oxide coating has a Vickers hardness of at least 50 HV, the rare earth-containing oxide coating is prevented from peeling from the substrate. Where the oxide coating has a surface roughness of up to 20 μm in centerline average roughness Ra, it becomes effective for preventing a powder metallurgical metal, cermet or ceramic product from deforming during sintering or heat treatment.

25

#### EXAMPLE

The following examples and comparative examples are provided to illustrate the invention, and are not intended to limit the scope thereof.

30

#### Example I

Carbon substrates having dimensions of 50×50×5 mm were furnished. In Examples 1 to 6, the surface of the substrate was roughened by blasting, following which rare earth-containing oxide particles having the compositions and average particle sizes indicated in Table 1 were plasma-sprayed in argon/hydrogen onto the substrate surface,

35

thereby coating the substrate with a layer of rare earth-containing oxide to form a coated member. Then the sprayed samples were heat treated in vacuum or in argon or roasted by an argon/hydrogen plasma flame, as indicated in Table 2.

In Examples 7 to 11, an oxide powder whose composition was shown in Table 1 was used and pressed into a preform having dimensions of 60×60×2-5 mm by a die pressing technique. The preform was then heat treated in an oxidizing atmosphere at 1700°C for 2 hours, obtaining a plate of rare earth oxide. The plate was attached to the substrate to produce a rare earth oxide-covered member.

In Comparative Examples 1 and 2, coated members were similarly produced under the conditions shown in Tables 1 and 2.

The physical properties of the coated members were measured. The results are shown in Table 1. The compositions were measured using inductively coupled plasma spectroscopy (Seiko SPS-4000). The average particle sizes were measured by a laser diffraction method (Nikkiso FRA). The physical properties of the thermally sprayed coatings and heat treated preforms were also measured, with the results given below in Table 2. The thickness of the thermally sprayed coating was determined from a cross-sectional image of the coating taken with an optical microscope. The surface roughness Ra was measured with a surface roughness gauge (SE3500K; Kosaka Laboratory, Ltd.) in accordance with JIS B0601. The Vickers hardness was measured with a digital micro-hardness meter (Matsuzawa SMT-7) in accordance with JIS R1610, after the surface was mirror finished.

Next, a tungsten carbide powder was mixed with 10 wt% of a cobalt powder and the mixture was pressed into a compact having dimensions of 10×40×3 mm. The compact was rested on the rare earth oxide-coated member (jig) and sintered in a low vacuum at 1,400°C for 2 hours. The sintering were conducted in a carbon heater furnace in such a pattern that the temperature was ramped up to 1,400°C at a rate of

300°C/h, held at that temperature for a predetermined length of time, then lowered at a rate of 400°C/h. This sintering cycle was repeated twice, after which the coated member was examined for peeling of the rare earth oxide coating from the substrate, seizure of the coated member to the sample being sintered, and warpage of the sample. The results are shown in Table 3.

10

Table 1

	Composition (weight ratio)	Average particle size ( $\mu\text{m}$ )	Substrate material	Substrate density ( $\text{g/cm}^3$ )
Example 1-3	$\text{Yb}_2\text{O}_3$	40	C	1.7
Example 4-6	$\text{Er}_2\text{O}_3$	50	C	1.7
Example 7	$\text{Yb}_2\text{O}_3$	40	C	1.7
Example 8	$\text{Dy}_2\text{O}_3$	50	C	1.7
Example 9	$\text{Sm}_2\text{O}_3$	40	C	1.7
Example 10	$\text{Gd}_2\text{O}_3$	40	C	1.7
Example 11	$\text{Gd}_2\text{O}_3 + \text{Al}_2\text{O}_3$ (50:50)	40	C	1.7
Comparative Example 1	$\text{Al}_2\text{O}_3$	40	C	1.7
Comparative Example 2	$\text{Y}_2\text{O}_3$	60	C	1.7

**Table 2**

	Coating layer	Coating thickness (mm)	Heat treating conditions	Before heat treatment		After heat treatment	
				Roughness Ra (μm)	Hardness (HV)	Roughness Ra (μm)	Hardness (HV)
Example 1	Yb <sub>2</sub> O <sub>3</sub> sprayed	0.20	no	7	80	7	80
Example 2	Yb <sub>2</sub> O <sub>3</sub> sprayed	0.15	1500° C in vacuum			5	100
Example 3	Yb <sub>2</sub> O <sub>3</sub> sprayed	0.30	plasma flame in air			2	200
Example 4	Er <sub>2</sub> O <sub>3</sub> sprayed	0.15	no	8	65	8	65
Example 5	Er <sub>2</sub> O <sub>3</sub> sprayed	0.20	1600° C in Ar			6	85
Example 6	Er <sub>2</sub> O <sub>3</sub> sprayed	0.20	plasma flame in air			3	160
Example 7	Yb <sub>2</sub> O <sub>3</sub> preform	5	1700° C in air	3	45	0.5	1015
Example 8	Dy <sub>2</sub> O <sub>3</sub> preform	3	1700° C in air	4	40	0.3	650
Example 9	Sm <sub>2</sub> O <sub>3</sub> preform	2	1700° C in air	6	38	1	205
Example 10	Gd <sub>2</sub> O <sub>3</sub> preform	4	1700° C in air	7	48	1.5	310
Example 11	Gd <sub>2</sub> O <sub>3</sub> +Al <sub>2</sub> O <sub>3</sub> preform	5	1700° C in air	5	35	0.8	2130
Comparative Example 1	Al <sub>2</sub> O <sub>3</sub> paste coated	0.2	no	25	30	25	30
Comparative Example 2	Y <sub>2</sub> O <sub>3</sub> preform	3	no	5	40	5	40



Table 3

	Coating layer appearance	Seizure of sample	Warpage of sample
Example 1	no peeling	no	0.2 mm
Example 2	no peeling	no	0.1 mm
Example 3	no peeling	no	0.1 mm
Example 4	no peeling	no	0.3 mm
Example 5	no peeling	no	0.2 mm
Example 6	no peeling	no	0.1 mm
Example 7	no peeling	no	0.1 mm
Example 8	no peeling	no	0.1 mm
Example 9	no peeling	no	0.1 mm
Example 10	no peeling	no	0.1 mm
Example 11	no peeling	no	0.2 mm
Comparative Example 1	peeled	seized	1 mm
Comparative Example 2	crazed	no	0.5 mm

The jigs of Examples 1 to 11 remained unchanged after  
5 heat treatment in a carbon heater furnace relative to before  
treatment. On sintering, the samples did not seize to the  
jigs and deformed little. By contrast, following heat  
treatment in a carbon heater furnace, the jigs of Comparative  
Examples 1 and 2 underwent surface crazing or oxide  
10 delamination, leading to corrosion. In Comparative Example  
1, the sample seized to the jig and deformed noticeably.

#### Example II

There were furnished matrix materials: carbon,  
15 molybdenum, tantalum, tungsten, aluminum, stainless steel,  
sintered alumina and sintered yttria (the latter two being  
oxide ceramics) having different coefficients of thermal  
expansion as shown in Table 4. The matrix materials were  
machined into substrates having dimensions of 50×50×5 mm.

The surface of the substrate was roughened by blasting, following which rare earth-containing oxide particles were plasma-sprayed in argon/hydrogen onto the substrate surface, thereby forming a spray coated member with a rare

5 earth-containing oxide coating of 200  $\mu\text{m}$  thick.

It is noted that the coefficient of thermal expansion of substrate shown in Table 4 was measured on a prism specimen of 3x3x15 mm in an inert atmosphere according to a differential expansion method using a thermomechanical  
10 analyzer TMA8310 (Rigaku Denki K.K.). The measurement is an average coefficient of thermal expansion over the temperature range of 20 to 100°C.

In Examples 12-17 and 21-27 and Comparative Examples 3-5, a  $\text{Er}_2\text{O}_3$  or  $\text{Yb}_2\text{O}_3$  power was used in spraying. In Example  
15 18,  $\text{Yb}_2\text{O}_3$  powder and  $\text{Zr}_2\text{O}_3$  powder were mixed in a  $\text{Yb}_2\text{O}_3$  :  $\text{Zr}_2\text{O}_3$  weight ratio of 80 wt%: 20 wt% to form a mixture, which was sprayed. In Example 19, a powder in which 90 wt% of  $\text{Yb}_2\text{O}_3$  was chemically combined with 10 wt% of  $\text{Zr}_2\text{O}_3$  was used in spraying. In Example 20,  $\text{Yb}_2\text{O}_3$  powder was sprayed to form a  
20 coating of 100  $\mu\text{m}$  thick, after which a  $\text{Y}_2\text{O}_3$  coating of 100  $\mu\text{m}$  thick was formed thereon by spraying.

These spray coated members based on the substrates having different coefficients of thermal expansion were set in a carbon heater furnace. The furnace was evacuated to  
25 vacuum, heated in a nitrogen atmosphere up to 800°C at a rate of 400°C/h, evacuated to vacuum again, and heated in a vacuum atmosphere of  $10^{-2}$  Torr up to a predetermined temperature at a rate of 400°C/h. After holding at the temperature for a certain time, the heater was turned off. Argon was  
30 introduced at 1000°C, after which the furnace was cooled down to room temperature at a rate of 500°C/h. This heating and cooling cycle was repeated 10 times. After the thermal cycling test, the coated members were observed under a microscope with a magnifying power of 100x to see whether the  
35 sprayed coating peeled from the substrate. The results are shown in Table 5.

Table 4

	Sprayed coating composition	Substrate material	Substrate density (g/cm <sup>3</sup> )	Substrate coefficient of thermal expansion (1/K)
Example 12	Er <sub>2</sub> O <sub>3</sub>	C	1.70	4.2×10 <sup>-6</sup>
Example 13	Er <sub>2</sub> O <sub>3</sub>	C	1.75	5.2×10 <sup>-6</sup>
Example 14	Er <sub>2</sub> O <sub>3</sub>	C	1.82	6×10 <sup>-6</sup>
Example 15	Yb <sub>2</sub> O <sub>3</sub>	C	1.70	4.2×10 <sup>-6</sup>
Example 16	Yb <sub>2</sub> O <sub>3</sub>	C	1.75	5.2×10 <sup>-6</sup>
Example 17	Yb <sub>2</sub> O <sub>3</sub>	C	1.82	6×10 <sup>-6</sup>
Example 18	Yb <sub>2</sub> O <sub>3</sub> +Zr <sub>2</sub> O <sub>3</sub> (80 wt%:20 wt%)	C	1.82	6×10 <sup>-6</sup>
Example 19	Yb <sub>2</sub> O <sub>3</sub> +Al <sub>2</sub> O <sub>3</sub> (90 wt%:10 wt%)	C	1.70	4.2×10 <sup>-6</sup>
Example 20	upper Y <sub>2</sub> O <sub>3</sub> / lower Yb <sub>2</sub> O <sub>3</sub> (100 μm/100 μm)	C	1.75	5.2×10 <sup>-6</sup>
Example 21	Yb <sub>2</sub> O <sub>3</sub>	Mo	10.2	5.3×10 <sup>-6</sup>
Example 22	Yb <sub>2</sub> O <sub>3</sub>	Ta	16.6	6.3×10 <sup>-6</sup>
Example 23	Yb <sub>2</sub> O <sub>3</sub>	W	19.1	4.5×10 <sup>-6</sup>
Example 24	Yb <sub>2</sub> O <sub>3</sub>	Al	2.7	23.1×10 <sup>-6</sup>
Example 25	Yb <sub>2</sub> O <sub>3</sub>	stainless steel	8.2	14.7×10 <sup>-6</sup>
Example 26	Yb <sub>2</sub> O <sub>3</sub>	sintered Al <sub>2</sub> O <sub>3</sub>	3.97	8.6×10 <sup>-6</sup>
Example 27	Yb <sub>2</sub> O <sub>3</sub>	sintered Y <sub>2</sub> O <sub>3</sub>	4.50	9.3×10 <sup>-6</sup>
Comparative Example 3	Er <sub>2</sub> O <sub>3</sub>	C	1.74	1.5×10 <sup>-6</sup>
Comparative Example 4	Yb <sub>2</sub> O <sub>3</sub>	C	1.74	1.5×10 <sup>-6</sup>
Comparative Example 5	Yb <sub>2</sub> O <sub>3</sub>	C	1.60	2.5×10 <sup>-6</sup>

Table 5

	Test temp. (°C)	Holding time (hr)	1st	2nd	3rd	4th	5th	6th	7th	8th	9th	10th	Observation after thermal cycling test of 10 cycles
EX 12	1400	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 13	1400	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 14	1400	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 15	1500	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 16	1500	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 17	1500	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 18	1500	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 19	1500	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 20	1500	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 21	1600	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 22	1600	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 23	1600	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 24	500	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 25	900	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 26	1400	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
EX 27	1500	4	pass	pass	pass	pass	pass	pass	pass	pass	pass	pass	not peeled
CE 3	1400	4	pass	pass	reject	reject	reject	reject	reject	reject	reject	reject	peeled in 3rd cycle
CE 4	1500	4	pass	pass	pass	pass	pass	reject	reject	reject	reject	reject	peeled in 6th cycle
CE 5	1500	4	pass	pass	pass	pass	pass	pass	pass	pass	reject	reject	peeled in 9th cycle

5       The spray coated members of Examples 12 to 27 remained  
 unchanged after the thermal cycling test of 10 cycles in  
 vacuum in a carbon heater furnace relative to before  
 treatment, with no evidence of peeling of the coating from  
 the substrate observed. In the coated members of Comparative  
 Examples 3 to 5, the coating peeled from the substrate during  
 10   the thermal cycling test. It is demonstrated that when a  
 coating is sprayed on a substrate having a coefficient of  
 thermal expansion of at least  $4 \times 10^{-6}$  (1/K), the coated member  
 is durable in that the coating do not peel from the substrate  
 during thermal cycling.

### Example III

There were furnished matrix materials: carbon, molybdenum, alumina ceramic, mullite ceramic and silicon carbide. The matrix materials were machined into substrates having dimensions of 50×50×5 mm. The surface of the substrate was roughened by blasting. In Comparative Examples 6-10, complex oxide particles containing yttrium or lanthanoid element and aluminum were plasma-sprayed in argon/hydrogen onto the substrate surface, thereby forming a spray coated member with an oxide coating of 100 μm thick.

To prevent reaction with the carbon substrate and to enhance the bonding force to the substrate, in Examples 28-32, tungsten or silicon particles were plasma-sprayed in argon/hydrogen as an interlayer to form a metal coating of 50 μm thick. On the metal coating, Yb<sub>2</sub>O<sub>3</sub> particles, Gd<sub>2</sub>O<sub>3</sub> particles, or complex oxide particles containing Y, Yb or Gd and Al were plasma-sprayed in argon/hydrogen, thereby forming a dual spray coated member having a total coating thickness of 100 μm.

In Examples 33-39, particles of Y, Yb or Zr oxide, or a mixture of particles of Yb or Al oxide and metallic W particles were plasma-sprayed in argon/hydrogen to form a coating of 50 μm thick. On the coating, Yb<sub>2</sub>O<sub>3</sub> particles, Gd<sub>2</sub>O<sub>3</sub> particles, or complex oxide particles containing Yb, Gd or Y and Al were plasma-sprayed in argon/hydrogen, thereby forming a dual spray coated member having a total coating thickness of 100 μm.

In Comparative Examples 11-13, spray coated members having a coating thickness of 100 μm were prepared in the same manner as in Comparative Examples 6-10 except that Y<sub>2</sub>O<sub>3</sub> particles, Al<sub>2</sub>O<sub>3</sub> particles, or particles of Y+Zr were used.

In Comparative Example 14, tungsten particles were plasma-sprayed in argon/hydrogen to form a metal coating of 50 μm thick. On the metal coating, Y<sub>2</sub>O<sub>3</sub> particles were plasma-sprayed in argon/hydrogen, thereby forming a dual

spray coated member having a total coating thickness of 100  $\mu\text{m}$ .

The thickness of sample coating films was measured by sectioning the coating, polishing the section, and observing under an electron microscope with a low magnifying power.

The samples of Examples 28-39 and Comparative Examples 6-14 were heated in a vacuum atmosphere of  $10^{-2}$  Torr to a temperature of  $1,550^{\circ}\text{C}$  at a rate of  $400^{\circ}\text{C/h}$ . After holding at the temperature for 2 hours, the heater was turned off.

Argon was introduced at  $1000^{\circ}\text{C}$ , after which the furnace was cooled down to room temperature at a rate of  $500^{\circ}\text{C/h}$ .

Next, a tungsten carbide powder was mixed with 10 wt% of a cobalt powder and the mixture was pressed into a compact having a diameter of 20 mm and a thickness of 10 mm. The compact was rested on the coated member which had been heat treated at  $1,550^{\circ}\text{C}$ . This was placed in a carbon heater furnace. The furnace was evacuated to vacuum, heated in a nitrogen atmosphere up to  $800^{\circ}\text{C}$  at a rate of  $400^{\circ}\text{C/h}$ , evacuated to vacuum again, and heated in a vacuum atmosphere of  $10^{-2}$  Torr up to a predetermined temperature at a rate of  $400^{\circ}\text{C/h}$ . After holding at the temperature for 2 hours, the heater was turned off. Argon was introduced at  $1000^{\circ}\text{C}$ , after which the furnace was cooled down to room temperature at a rate of  $500^{\circ}\text{C/h}$ . This heating and cooling cycle was repeated 5 times, provided that a fresh compact was rested on the coated member on the start of each cycle. After the thermal cycling test, the coated members were observed to see whether the sprayed complex oxide coating peeled from the substrate due to seizure of the compact being fired. The results are shown in Table 7.

Table 6

	Topcoat composition	Intermediate coating layer composition	Substrate material
Example 28	$\text{Yb}_2\text{O}_3$ (100 wt%)	W (100 wt%)	C
Example 29	$\text{Gd}_2\text{O}_3$ (100 wt%)	W (100 wt%)	C
Example 30	$\text{Y}_2\text{O}_3+\text{Al}_2\text{O}_3$ (50 wt%+50 wt%)	W (100 wt%)	C
Example 31	$\text{Gd}_2\text{O}_3+\text{Al}_2\text{O}_3$ (70 wt%+30 wt%)	W (100 wt%)	C
Example 32	$\text{Yb}_2\text{O}_3+\text{Al}_2\text{O}_3$ (50 wt%+50 wt%)	Si (100 wt%)	C
Example 33	$\text{Y}_2\text{O}_3+\text{Al}_2\text{O}_3$ (50 wt%+50 wt%)	$\text{Yb}_2\text{O}_3$ (100 wt%)	C
Example 34	$\text{Yb}_2\text{O}_3$ (100 wt%)	$\text{Y}_2\text{O}_3$ (100 wt%)	C
Example 35	$\text{Gd}_2\text{O}_3+\text{Al}_2\text{O}_3$ (60 wt%+40 wt%)	$\text{Yb}_2\text{O}_3$ (100 wt%)	C
Example 36	$\text{Yb}_2\text{O}_3+\text{Al}_2\text{O}_3$ (50 wt%+50 wt%)	$\text{Y}_2\text{O}_3+\text{ZrO}_2$ (70 wt%+30 wt%)	C
Example 37	$\text{Y}_2\text{O}_3+\text{Al}_2\text{O}_3$ (70 wt%+30 wt%)	$\text{Yb}_2\text{O}_3+\text{W}$ (40 wt%+60 wt%)	C
Example 38	$\text{Gd}_2\text{O}_3+\text{Al}_2\text{O}_3$ (50 wt%+50 wt%)	$\text{Al}_2\text{O}_3+\text{W}$ (60 wt%+40 wt%)	C
Example 39	$\text{Gd}_2\text{O}_3$ (100 wt%)	$\text{Yb}_2\text{O}_3$ (100 wt%)	C
Comparative Example 6	$\text{Y}_2\text{O}_3+\text{Al}_2\text{O}_3$ (50 wt%+50 wt%)	no	C
Comparative Example 7	$\text{Yb}_2\text{O}_3+\text{Al}_2\text{O}_3$ (70 wt%+30 wt%)	no	Mo
Comparative Example 8	$\text{Gd}_2\text{O}_3+\text{Al}_2\text{O}_3$ (60 wt%+40 wt%)	no	alumina
Comparative Example 9	$\text{Lu}_2\text{O}_3+\text{Al}_2\text{O}_3$ (60 wt%+40 wt%)	no	mullite
Comparative Example 10	$\text{Er}_2\text{O}_3+\text{Al}_2\text{O}_3$ (40 wt%+60 wt%)	no	SiC
Comparative Example 11	$\text{Y}_2\text{O}_3$ (100 wt%)	no	C
Comparative Example 12	$\text{Al}_2\text{O}_3$ (100 wt%)	no	C
Comparative Example 13	$\text{Y}_2\text{O}_3+\text{ZrO}_2$ (70 wt%+30 wt%)	no	C
Comparative Example 14	$\text{Y}_2\text{O}_3$ (100 wt%)	W (100 wt%)	C

Table 7

	Sintering temp. (° C)	1st	2nd	3rd	4th	5th	Observation after thermal cycling test
Example 28	1,450	pass	pass	pass	pass	pass	not peeled
Example 29	1,450	pass	pass	pass	pass	pass	not peeled
Example 30	1,450	pass	pass	pass	pass	pass	not peeled
Example 31	1,450	pass	pass	pass	pass	pass	not peeled
Example 32	1,450	pass	pass	pass	pass	pass	not peeled
Example 33	1,450	pass	pass	pass	pass	pass	not peeled
Example 34	1,450	pass	pass	pass	pass	pass	not peeled
Example 35	1,450	pass	pass	pass	pass	pass	not peeled
Example 36	1,450	pass	pass	pass	pass	pass	not peeled
Example 37	1,450	pass	pass	pass	pass	pass	not peeled
Example 38	1,450	pass	pass	pass	pass	pass	not peeled
Example 39	1,450	pass	pass	pass	pass	pass	not peeled
Comparative Example 6	1,350	pass	pass	reject	reject	reject	peeled in 3rd cycle
Comparative Example 7	1,350	pass	pass	reject	reject	reject	peeled in 3rd cycle
Comparative Example 8	1,350	pass	pass	reject	reject	reject	peeled in 3rd cycle
Comparative Example 9	1,350	pass	pass	reject	reject	reject	peeled in 3rd cycle
Comparative Example 10	1,350	pass	pass	reject	reject	reject	peeled in 3rd cycle
Comparative Example 11	1,350	reject	reject	reject	reject	reject	peeled in 1st cycle
Comparative Example 12	1,350	reject	reject	reject	reject	reject	peeled in 1st cycle
Comparative Example 13	1,350	reject	reject	reject	reject	reject	peeled in 1st cycle
Comparative Example 14	1,450	pass	pass	reject	reject	rej ct	peeled in 3rd cycle



In the spray coated members of Examples 28-39, no delamination of the coating was observed after five consecutive tests of sintering WC/Co cemented carbide in a vacuum atmosphere in a carbon heater furnace. In contrast, 5 in the spray coated members of Comparative Examples 6-14, delamination of the coating occurred in five consecutive sintering tests due to seizure of WC/Co specimens. It is thus demonstrated that a spray coated member in the form of a substrate coated with a layer containing a complex oxide of 10 yttrium, lanthanoid and aluminum is durable because the peeling of the sprayed coating caused by seizure of WC/Co cemented carbide specimens is minimized. Durability is further enhanced using an interlayer containing a refractory metal, a lanthanoid oxide or a mixture of a refractory metal 15 and a lanthanoid oxide.

#### Example IV

To examine how the durability of a coated member is affected by the coefficient of thermal expansion of a 20 substrate and the hardness and composition of an upper coating layer, a thermal cycling test simulating the sintering of cemented carbide material was carried out for observing whether the coating layer was peeled. The test and its results are described below.

25 There were furnished carbon matrix materials having different coefficients of thermal expansion as shown in Table 8. The matrix materials were machined into substrates having dimensions of 50×50×5 mm. The surface of the substrate was roughened by blasting. Oxide particles were plasma-sprayed 30 in argon/hydrogen onto the substrate surface and heat treated, thereby forming a spray coated member with a coating of 100 μm thick having a certain hardness and roughness (Examples 40-43 and Comparative Examples 17-19). In Comparative Examples 15 and 16, an oxide powder was combined 35 with a binder and water to form a paste, which was coated onto the substrate surface to form a coated member with a coating having a certain hardness and roughness.

The samples of Examples 40-43 and Comparative Examples 15-19 were heated in a vacuum atmosphere of  $10^{-2}$  Torr to a temperature of  $1,550^{\circ}\text{C}$  at a rate of  $400^{\circ}\text{C/h}$ . After holding at the temperature for 2 hours, the heater was turned off.

5 Argon was introduced at  $1000^{\circ}\text{C}$ , after which the furnace was cooled down to room temperature at a rate of  $500^{\circ}\text{C/h}$ . This procedure was intended for water removal and for preventing premature peeling of the coating layer.

Next, a tungsten carbide powder was mixed with 10 wt%  
10 of a cobalt powder and the mixture was pressed into a cemented carbide-forming compact having a diameter of 20 mm and a thickness of 10 mm. The compact was rested on the coated member which had been heat treated at  $1,550^{\circ}\text{C}$ . This was placed in a carbon heater furnace. The furnace was  
15 evacuated to vacuum, heated in a nitrogen atmosphere up to  $800^{\circ}\text{C}$  at a rate of  $400^{\circ}\text{C/h}$ , evacuated to vacuum again, and heated in a vacuum atmosphere of  $10^{-2}$  Torr up to  $1,450^{\circ}\text{C}$  (sintering temperature for cemented carbide) at a rate of  $400^{\circ}\text{C/h}$ . After holding at the temperature for 2 hours, the  
20 heater was turned off. Argon was introduced at  $1000^{\circ}\text{C}$ , after which the furnace was cooled down to room temperature at a rate of  $500^{\circ}\text{C/h}$ . This heating and cooling cycle was repeated 10 times, provided that a fresh compact was rested on the coated member on the start of each cycle. After the thermal  
25 cycling test, the coated members were observed to see whether the coating layer peeled from the substrate. The results are shown in Table 9.

The coating layer peels through the following mechanism. Cobalt exudes from the bottom of the cemented  
30 carbide sample at the sintering temperature of  $1,450^{\circ}\text{C}$  and subsequently catches the coating layer during cooling for solidification, whereby the cemented carbide sample and the coating layer are seized together. When the cemented carbide sample is taken out of the coated member (jig) after  
35 resumption to room temperature, the coating layer is peeled so that the underlying carbon surface is exposed.

Example 40 and Comparative Examples 15 and 16 are to examine how durability varies with the hardness of the upper coating layer. For the same material ( $\text{Yb}_2\text{O}_3$ ), the higher the hardness of the upper coating layer, the better became the durability. Equivalent results were obtained from the other material ( $\text{Al}_2\text{O}_3$ ).

Example 41 and Comparative Example 17 are to examine how durability varies with the coefficient of thermal expansion of the substrate when the upper coating layer has the same hardness. For the same material ( $\text{Yb}_2\text{O}_3$ ) and the same hardness, the higher the coefficient of thermal expansion of the substrate, the better became the durability.

Examples 42 and 43 and Comparative Examples 18 and 19 are to examine how durability varies with the presence or absence of the intermediate coating layer and with the composition of the coating layer. Those coated members having an intermediate coating layer of  $\text{Yb}_2\text{O}_3$  or  $\text{ZrO}_2$  and an upper coating layer of  $\text{Y}_2\text{O}_3 + \text{Al}_2\text{O}_3$  were fully durable in that no peeling occurred after ten thermal cycling tests.

It is evident that by using an upper coating layer having a high hardness and a substrate having a high coefficient of thermal expansion, and selecting as the upper coating layer a material unsusceptible to seizure of samples to be sintered, a carbon-base setter is obtainable which remains durable when used in the sintering of cemented carbide samples to be sintered at high temperatures of at least  $1400^\circ\text{C}$ .

**Table 8**

	Upper coating layer (weight ratio)	Intermediate coating layer (weight ratio)	Upper coating layer hardness (HV)	Upper coating layer roughness Ra ( $\mu\text{m}$ )	Substrate	Substrate's coefficient of thermal expansion
Example 40	sprayed $\text{Yb}_2\text{O}_3$ (100 wt%)	-	80	7	C	$4.2 \times 10^{-6}$
Comparative Example 15	paste coated $\text{Yb}_2\text{O}_3$ (100 wt%)	-	35	10	C	$4.2 \times 10^{-6}$
Comparative Example 16	paste coated $\text{Al}_2\text{O}_3$ (100 wt%)	-	30	25	C	$4.2 \times 10^{-6}$
Example 41	sprayed $\text{Yb}_2\text{O}_3$ (100 wt%)	-	80	7	C	$6 \times 10^{-6}$
Comparative Example 17	sprayed $\text{Yb}_2\text{O}_3$ (100 wt%)	-	80	7	C	$1.5 \times 10^{-6}$
Example 42	sprayed $\text{Y}_2\text{O}_3 + \text{Al}_2\text{O}_3$ (50+50 wt%)	sprayed $\text{Yb}_2\text{O}_3$ (100 wt%)	100	6	C	$6 \times 10^{-6}$
Example 43	sprayed $\text{Y}_2\text{O}_3 + \text{Al}_2\text{O}_3$ (30+70 wt%)	sprayed $\text{ZrO}_2$ (100 wt%)	100	6	C	$6 \times 10^{-6}$
Comparative Example 18	sprayed $\text{Y}_2\text{O}_3 + \text{Al}_2\text{O}_3$ (50+50 wt%)	-	100	6	C	$6 \times 10^{-6}$
Comparative Example 19	sprayed $\text{Y}_2\text{O}_3$ (100 wt%)	sprayed W (100 wt%)	100	6	C	$6 \times 10^{-6}$

**Table 9**

	Sintering temp. ( $^{\circ}\text{C}$ )	1st	2nd	3rd	4th	5th	10th	Peeling after thermal cycling tests
Example 40	1450	pass	pass	pass	pass	reject	reject	peeled in 5th test
Comparative Example 15	1450	reject	--	--	--	--	--	peeled in 1st test
Comparative Example 16	1450	reject	--	--	--	--	--	peeled in 1st test
Example 41	1450	pass	pass	pass	pass	pass	pass	peeled in 7th test
Comparative Example 17	1450	pass	pass	reject	--	--	--	peeled in 3rd test
Example 42	1450	pass	pass	pass	pass	pass	pass	not peeled
Example 43	1450	pass	pass	pass	pass	pass	pass	not peeled
Comparative Example 18	1450	pass	pass	reject	--	--	--	peeled in 3rd test
Comparative Example 19	1450	pass	pass	reject	--	--	--	peeled in 3rd test

Japanese Patent Application Nos. 2002-336769,  
2002-356171 and 2003-089797 are incorporated herein by  
reference.

Although some preferred embodiments have been  
5 described, many modifications and variations may be made  
thereto in light of the above teachings. It is therefore to  
be understood that the invention may be practiced otherwise  
than as specifically described without departing from the  
scope of the appended claims.

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